



## Technical Memorandum

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To:

From:

Date: July 25, 2007

Subject: ODOT Contract No. 16902 – I-5 Trade Corridor Study Phase II  
Technical Memorandum, Option Package 7

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### TECHINICAL MEMORANDUM, OPTION PACKAGE 7

(Insert objective)

#### Option Description

##### ROADWAY

##### **Four-Lane Bridge**

The proposed four-lane bridge will provide one High Occupancy Vehicle (HOV) and one General Purpose (GP) lane for each direction. It has 12' shoulder on both sides and 20' center median for a total width of 92 feet. It is located on the west side of the existing I-5 corridor starting from Victory Boulevard and terminating just south of Evergreen Bridge.

The bridge mainline carrying the HOV lanes begins on the north side of Victory Boulevard with its center matching the existing I-5 centerline. It crosses over Interstate-5 (I-5), Highway 99 and Expo Road. The existing I-5 northbound on-ramp at Victory Blvd. will be widened into two lanes to accommodate the proposed northbound GP lane that will cross over I-5 and then merge with the mainline bridge at Expo Center. An exit ramp will be provided for the southbound GP lane that will split into two lanes, one lane goes to Expo road and the other lane merges into the existing I-5. As shown on the plan, the existing I-5 will be widened to accommodate the additional 2 HOV lanes, 2 GP lanes and the existing 6 lanes.

A bus access ramp is proposed at Expo Center Station to serve City of Vancouver southbound and northbound bus service routes. In addition, a ramp is also provided southbound to City of Portland. The existing private road where the bus access is being proposed will be improved and converted into a public road to improve traffic circulation.



## Technical Memorandum

The existing I-5 connections at Hayden Island will be eliminated to relieve congestion on this area. Conversely, a split diamond interchange will be built to access Hayden Island through the new four-lane bridge. Tomahawk Island Drive will be extended thru and under I-5 with signalized intersections at both ramps. The entrance and exit ramps at Hayden Island Drive intersections will also be signalized to allow and control all directional traffic movements.

The four-lane bridge will cross the Columbia River with an elevation meeting the existing navigational clearance of the Interstate Bridge. It will go over the existing railroad and SR 14 interchange and touch down south of Evergreen Bridge. A northbound exit ramp is provided for the SR 14 eastbound and Sixth Avenue westbound connections. Furthermore, a southbound on-connection from Washington Street is proposed and a southbound off-connection with an over-crossing is designed to serve Sixth Avenue. All existing SR-14 and I-5 interchange connections will remain.

The affected area of I-5 where the proposed bridge ends will be widened on both sides to accommodate the additional lanes as a result of this improvement. The said widening will not impact the existing hospital on the historic reserve area, however, its road adjacent to the highway will be affected.

These proposed four-lane bridge terminates just south of Evergreen with its new lanes designed to conform to the proposed development of the Mill Plain interchange.

### Mill Plain to SR500

Between Mill Plain Blvd. and SR500 in Vancouver, the proposed design reconfigures the existing interchanges to eliminate the number of weaving sections on the freeway. The freeway remains a six through lane section with additional lanes added as auxiliary lanes between interchanges where the space between ramps is inadequate to provide for a merge and a diverge from the highway. The interchange improvements are accomplished primarily by braiding the on/off ramps. Construction of the braided ramps will require replacement of the overpasses for 29<sup>th</sup> St. and 33<sup>rd</sup> St., and widening of the Mill Plain and McLaughlin overcrossings.

Interchanges were modified based upon the schematic design developed at a workshop held with DOT and consultant team members on June 29, 2001. The design concept included braiding most of the ramps to and from the existing interchanges. Ramps to be braided include:

#### Northbound

- Fourth Plain on-ramp with SR500 off-ramp: The new diverge point for the SR500 off-ramp would begin on the north side of the Fourth Plain overpass. The Fourth Plain on-ramp would pass over the SR500 off-ramp, merging with the highway near the 29<sup>th</sup> Street overpass. The Fourth Plain on-ramp would also have a split to allow traffic to decide between accessing I-5 Northbound or SR500 Eastbound. Braiding of these ramps will require reconstruction of the 29<sup>th</sup> St. and 33<sup>rd</sup> St. overpasses.

#### Southbound

- SR500 on-ramp with Fourth Plain off-ramp: The diverge point for the Fourth Plain off-ramp would be moved to the area between the 39<sup>th</sup> St. off-ramp and the SR500 overpass.



## Technical Memorandum

The new ramp would align to the west side of the SR500 on-ramp, cross under the 39<sup>th</sup> St. on-ramp, and parallel the highway to connect to the existing interchange area. The design currently includes a connection between SR500 and Fourth Plain Blvd via a short weaving area. This weave takes place within the same zone that includes the SR500 to mainline weave and may negate the advantages of braiding the ramps. As a result, further study of the ramp configuration is recommended during the subsequent alternatives analysis to determine the need for this connection and, if warranted, whether the correct design approach is to braid the ramps at this location.

- Fourth Plain on-ramp with Mill Plain off-ramp: The diverge point for the Mill Plain off-ramp would be moved to approximately the same location as the existing Fourth Plain off-ramp diverge. The Mill Plain ramp would rise and crossover both the Fourth Plain on-ramp, which is left mostly unchanged from the existing configuration, and Fourth Plain Blvd. Much of this ramp will be on structure because of the need to clear Fourth Plain.
- Mill Plain on-ramp with SR14 off-ramp: To mitigate an existing short weave distance between the Mill Plain on-ramp and the SR14 off-ramp, the SR14 off-ramp diverge point would be move to the north edge of the Mill Plain underpass, braid over the Mill Plain on-ramp and make a connection to SR14 via the ramp included in the design for each of the river crossing options. The Mill Plain on-ramp would offer the option, via a mid-ramp split, to go to either I-5 southbound or SR14 eastbound.

This design segment also includes a connector between SR500 westbound and the 39<sup>th</sup> St. northbound on-ramp providing a direct connection between SR500 and northbound I-5.

During the I-5 HOV study, performed by Parsons Brinckerhoff, the observation was made that in Vancouver I-5 functions as both a regional and local connector. To improve performance of I-5, these two traffic types could be separated via a barrier creating, what is in affect, a bypass system through Vancouver for the regional traffic. This option would require additional widening of the freeway to accommodate all the lanes, but would eliminate the need to extensively braid the interchanges. Separation of the freeway would occur north of SR500 and south of SR14, although the river crossing options that include a bypass bridge could connect into the regional route. Lane configurations would likely include 2 lanes in each direction on the bypass (1 HOV and 1 General Purpose) and 2 lanes on the “local” system plus any necessary auxiliary lanes between interchanges. It is recommended that this option be revisited in future studies along with the braided ramp option shown.

### **STRUCTURE - X-LANE BRIDGE WITH LRT AND HOV ON LOWER DECK**

Main River Crossing



## ***Technical Memorandum***

### **STRUCTURE - X-LANE BRIDGE WITH LRT AND HOV ON LOWER DECK**

The x Lane Bridge with LRT& HOV alternative over the Columbia River is conceptualized as a double deck steel truss type with a vertical moveable span over the navigation channel. The Span layout could be comprised of (south bank to north bank) 260'-540'-270'-540'-540'-280' (Vertical lift Span)-320'. Currently the existing dual bridges provide a horizontal clearance of 263 feet between the lift spans piers over the main navigation channel. The lift span provides a 39-foot vertical clearance above the Columbia River Datum (also refereed to as zero gage or low water) when closed, and a maximum of 178 feet when fully raised. An increase vertical clearance of 58 feet is provided at the alternate barge channel beneath the bridge's fixed 531-foot truss span. South of the 531-foot span, a vertical clearance of 72 feet is provided between piers 6 and 7 and piers 7 and 8; these spans are outside of the maintained channel limits. The assumed profile of the x-lane bridge with LRT has the upper highway bridge deck elevation over the navigation channel at 145 feet in the closed position with LRT and HOV on the lower deck, approximately 45 feet lower (100' lower deck elevation in closed position). This is compared to the existing twin I-5 bridges which has a deck elevation of 45' feet(+/-) in the closed position. The 4 lane bridge will function with the exiting I-5 Bridges in operation. The new bridge is conceptualized to have a vertical lift moveable span, that when open will match existing vertical clearances. The deck elevation of 145 feet was assumed based on the vertical restriction associated with Person Airpark. The airpark airspace restriction is approximately at 175 feet; with the deck at 145 feet this should allow lights, signs and trucks to pass without infringing into the airspace. The two decks would open independently for lift span operations. Near the North Bank (Washington), the double deck bridge would transition to two independent bridges, as LRT facilities head toward downtown Vancouver, and the HOV and general-purpose lanes follow I-5. Both bridges in profile would travel over BNSF tracks.

#### **Major Considerations**

- *Superstructure Type* - The superstructure section could be a double deck truss, similar to the Marquam or Fremont bridges. The cross section could vary in depth from maximum depths over the interior piers to 1/10<sup>th</sup> the span length at mid-section (for a truss, arches and other types would have different depth to span ratios). A suggested depth to span ratio would be 1/8 at the pier, and 1/10 at midspan.
- *Column Type* - The river pier columns could match the type and spacing of the existing I-5 Bridges for the double deck truss Bridge Type.
- *Foundations* - The two end transition piers are on land at the riverbanks, and the interior piers are all in the river. For the river piers, a footing plan size of approximately 32 X 52 for the double deck truss could be required. Deep foundation elements may be either driven piles or drilled shafts. Larger diameter drilled shafts may be preferable to limit the construction impacts of noise and vibration normally associated with driven piles.



## ***Technical Memorandum***

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- *Construction Procedures* - The river piers may be constructed by conventional methods using cofferdams. This features braced sheet piling walls, driven piles, underwater tremie concrete pours, and extensive pumping of the water inside the cofferdam to allow construction of the remainder of the pier footing and columns in the dry. This foundation type features footings that are founded below the river bottom. Because contractors assume a high risk with this type of foundation construction, costs are generally high for the cofferdams.

The river piers may also be constructed as water level foundations. This foundation makes use of a precast concrete lost footing form. The form has a bottom and four sides approximately 15' high. The bottom has holes for piling or in this case, large diameter drilled shafts. The drilled shafts are installed with permanent casings from the water level down below the bottom of the river. The precast footing form is lifted and placed over the top of the shaft casings and supported by hangers from the casings. Underwater tremie concrete is placed in the bottom of the form to allow pumping out the water to construct the remainder of the footing in the dry. However, in this configuration, the bottom of footing is at a much higher elevation, requiring a smaller tremie pour due to the reduced hydrostatic head. This type of foundation is generally less costly, because the contractor risk is lowered.

The double deck truss superstructure construction would be fabricated off site, and finished spans barged to the site and lifted into position. A concrete deck would then be poured in place after the finished trusses are all in place.

### **Deviations from Standards**

### **ROW Impacts**

### **Costs**

Figure 1 – Option Schematic